Lecture 14 Precise Point Positioning (PPP)

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Galileo Masterclass Brazil (GMB) 2022

From Fundamentals to Signal and Data Processing



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Projeto financiado pela União Europeia

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August 2022



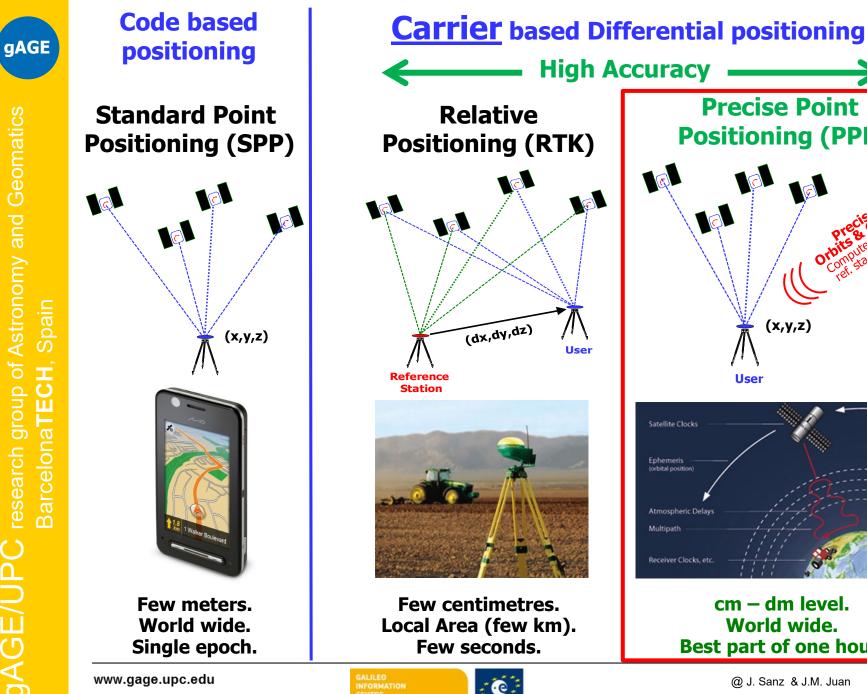
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- 2. Orbits and Clocks: Broadcast and Precise
- 3. Code and carrier measurements and modelling errors
- 4. Linear observation model for PPP
- 5. Parameter estimation: Floating Ambiguities
- 6. Carrier Ambiguity fixing concept: DD and undifferenced
- 7. Accelerating Filter convergence with accurate ionosphere

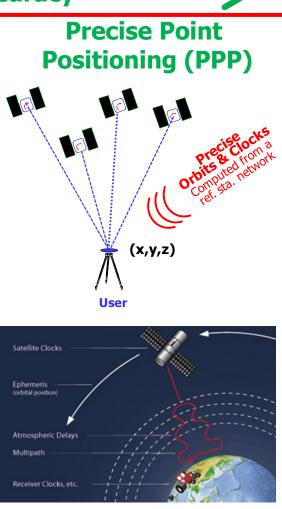
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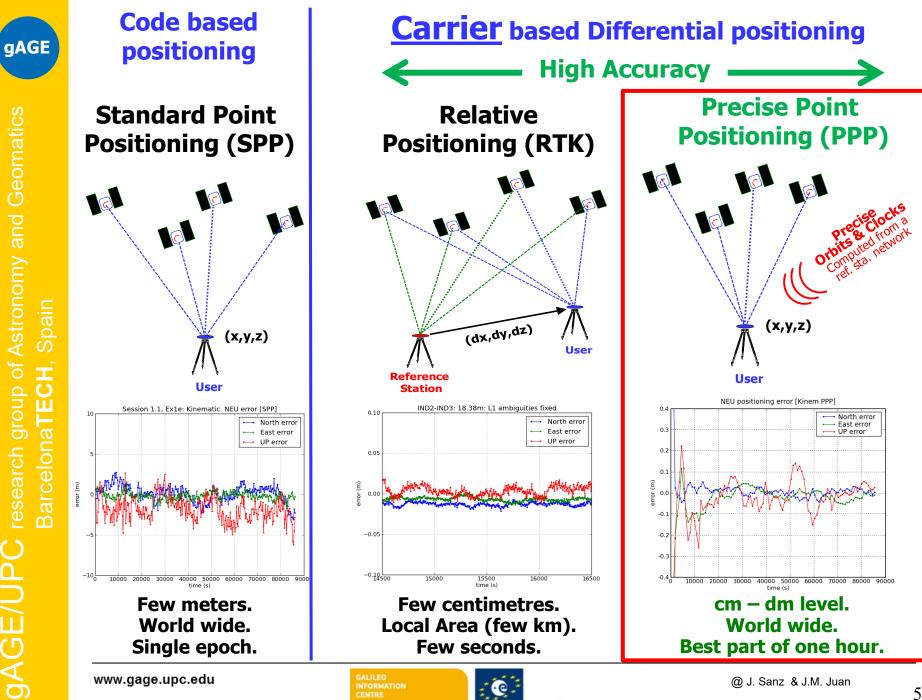
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cm – dm level. World wide. Best part of one hour.

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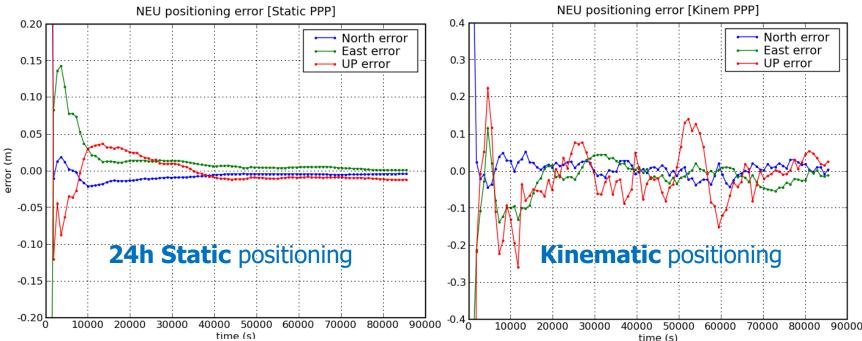


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The PPP technique allows **centimetre-level** accuracy to be achieved for static positioning and decimetre level, or better, for kinematic positioning, after the best part of one hour.



This high accuracy requires the use of code and carrier measurements and an accurate measurement modelling up to centimetre level or better.

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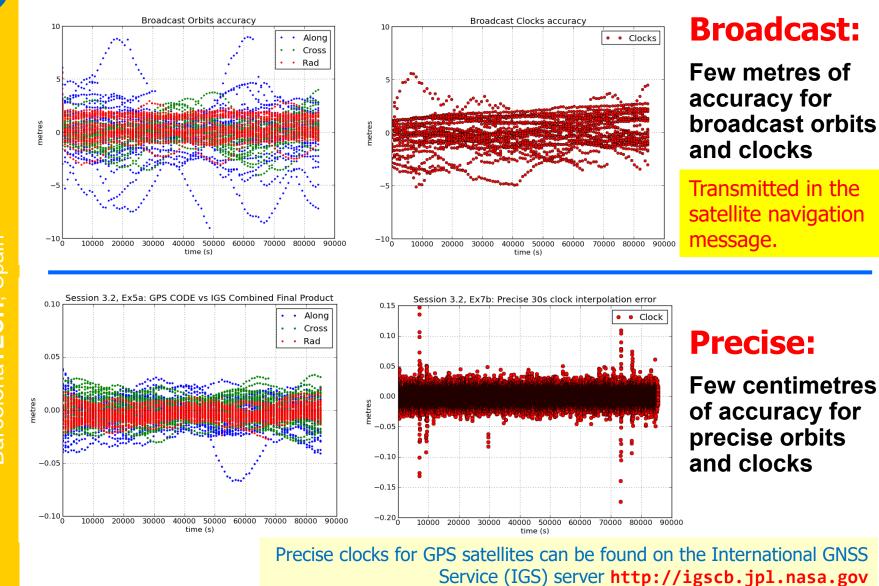
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Satellite Orbit and clock accuracies



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IGS Precise orbit and clock products: RMS accuracy, latency and sampling

Products	Broadcast	Ultra-rapid Predicted Observed		Rapid	Final	
(delay)	(real time)	(real time)	(3–9h)	(17–41 h)	(12–18d)	
Orbit GPS (sampling)	\sim 100 cm (\sim 2 h)	~5 cm (15 min)	~3 cm (15 min)	~2.5cm (15 min)	~ 2.5 cm (15 min)	
Glonass (sampling)					~5 cm (15 min)	
Clock GPS (sampling)	~5 ns (daily)	~3 ns (15 min)	$\sim \! 150 \mathrm{ps}$ (15 min)	~75 ps (5 min)	~75 ps (30 s)	
Glonass (sampling)					\sim TBD (15 min)	

http://igscb.jpl.nasa.gov/components/prods.html





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Computation of <u>satellite coordinates</u> from precise products.

Precise orbits for GPS satellites can be found on the International GNSS Service (IGS) server http://igscb.jpl.nasa.gov

Orbits are given by (x,y,z) coordinates with a sampling rate of 15 minutes. The satellite coordinates between epochs can be computed by polynomial interpolation. A 10th-order polynomial is enough for a centimetre level of accuracy with 15 min data.

$$P_{n}(x) = \sum_{i=1}^{n} y_{i} \frac{\prod_{j \neq i} (x - x_{j})}{\prod_{j \neq i} (x_{i} - x_{j})}$$

$$= y_{1} \frac{x - x_{2}}{x_{1} - x_{2}} \cdots \frac{x - x_{n}}{x_{1} - x_{n}} + \cdots$$

$$+ y_{i} \frac{x - x_{1}}{x_{i} - x_{1}} \cdots \frac{x - x_{i-1}}{x_{i} - x_{i-1}} \frac{x - x_{i+1}}{x_{i} - x_{i+1}} \cdots \frac{x - x_{n}}{x_{i} - x_{n}} + \cdots$$

$$+ y_{n} \frac{x - x_{1}}{x_{n} - x_{1}} \cdots \frac{x - x_{n-1}}{x_{n} - x_{n-1}}$$

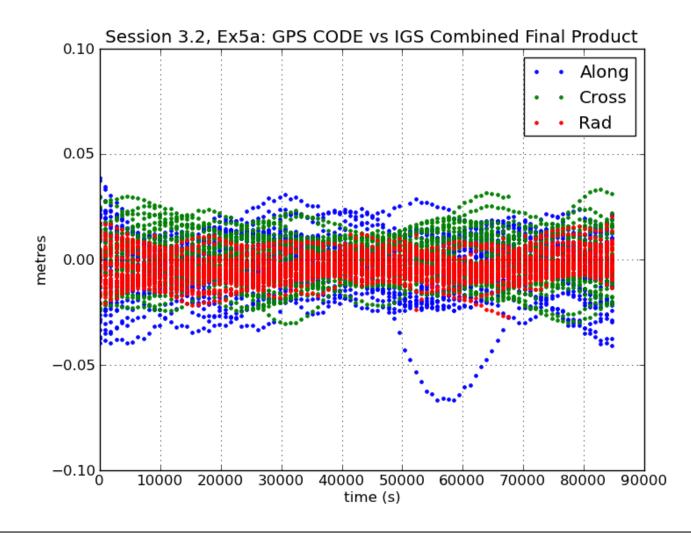
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IGS orbit and clock products (for PPP):

Discrepancy between the different centres



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Computation of <u>satellite clocks</u> from precise products

Precise clocks for GPS satellites can be found on the International GNSS Service (IGS) server http://igscb.jpl.nasa.gov

IGS is providing precise <u>orbits and clock files</u> with a sampling rate of <u>15 min</u>, as well as <u>precise clock files with a sample rate of 5 min</u> and 30 sec, in SP3 and CLK formats.

Some centres also provide GPS satellite clocks with a 5 sec sampling rate, like the les obtained from the Crustal Dynamics Data Information System (CDDIS) site.

Stable clocks with a sampling rate of 30 sec or higher can be interpolated with a first-order polynomial to a few centimetres of accuracy. Clocks with a lower sampling rate should not be interpolated, because clocks evolve as random walk processes.

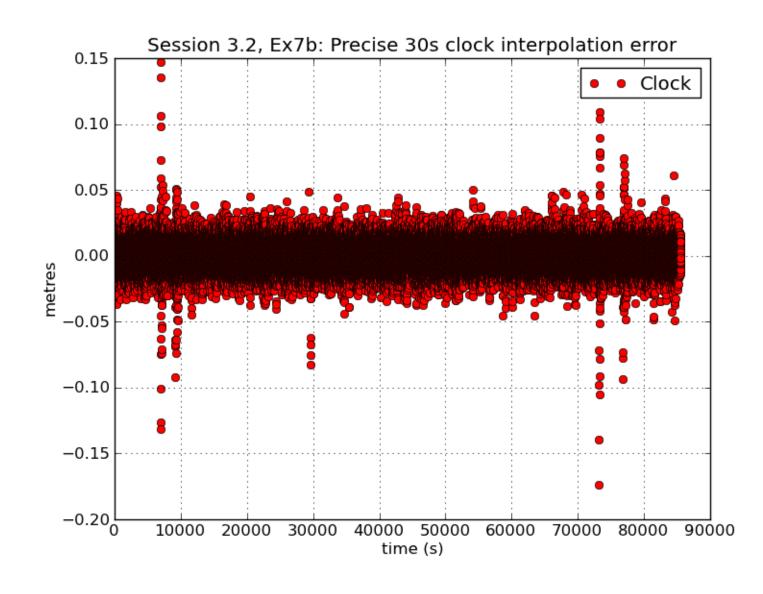
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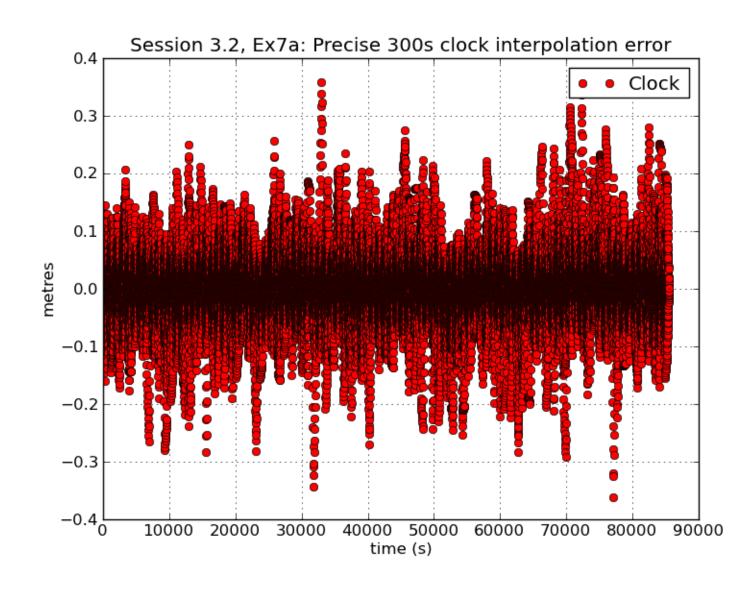


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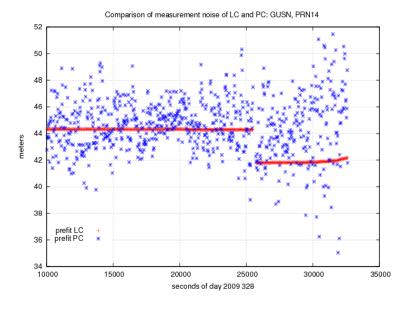
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Measurements: Code and carrier

For high-accuracy positioning, the carrier phase must be used, besides the code pseudorange.

The carrier measurements are very precise, typically at the level of a few millimetres, but contain unknown ambiguities which change every time the receiver locks the signal after a cycle slip.

Nevertheless, such ambiguities can be estimated in the navigation solution, together with the coordinates and other parameters.







Example 1: Standard Point Positioning (SPP)

Dotted Line V

Plot

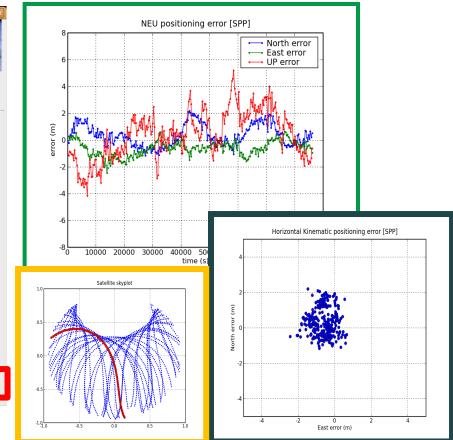
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A Plotting Results

	gLAB - Ver	sion 2.0.0	
eesa	gLA	B	magage/UP
cioning Analysis	Preferences	About	t
NEU positioning error	Horizontal positioning error	Zenith Tropospheric Delay	Ionospheric combinations
Dilution Of Precision	Satellite skyplot	Carrier phase ambiguities	Measur. Multipath/Noise
Model components	Prefit residuals	Postfit residuals	Orbit and Clock comparison
oal Graphic Parameters e : NEU positioning error	X-label : time (s)	Y-label : error (m)	Clear
Automatic Limits X-min : vidual Plot(s) Configuration-	X-max :	Y-min : Y-m	nax :
Dist No. 1		Diet No. 2	Dist No. 4

Positioning with few meters of error is achieved **in kinematic SPP mode**.

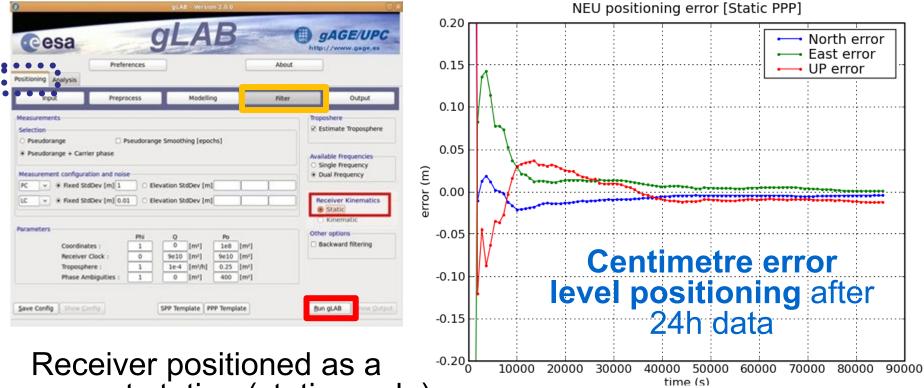
- Receiver navigated as a rover in <u>pure</u> kinematic mode.
- <u>Single frequency C1 code is used.</u>
- Broadcast orbits and clocks.





Precise Point Positioning: Static

From default configuration of [PPP Template], Select Static in the [Filter] panel. Run gLAB and plot results



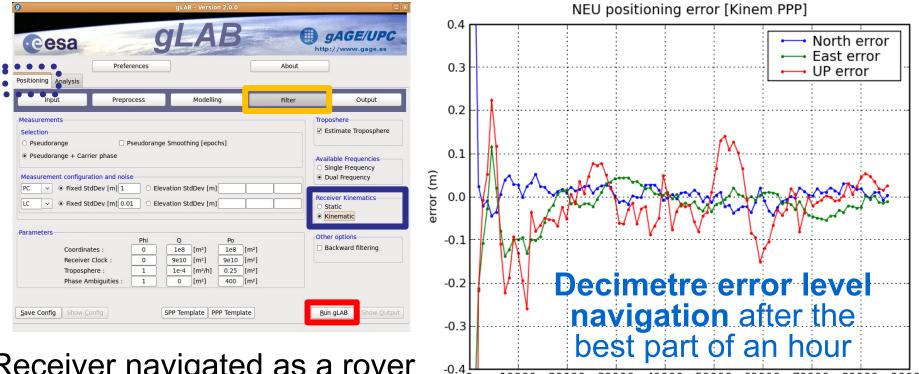
permanent station (static mode)





Precise Point Positioning: Kinematic

From default configuration of [PPP Template], Select <u>kinematics</u> in the [Filter] panel. Run gLAB and plot results



10000

20000

30000

Receiver navigated as a rover in a pure kinematic mode.





40000

time (s)

50000

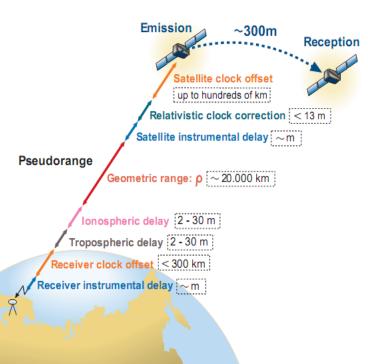
60000

70000

80000

90000

PPP Model components



We are going to review first the measurements modelling for the Standard Point Positioning (SPP). A brief summary is given next.

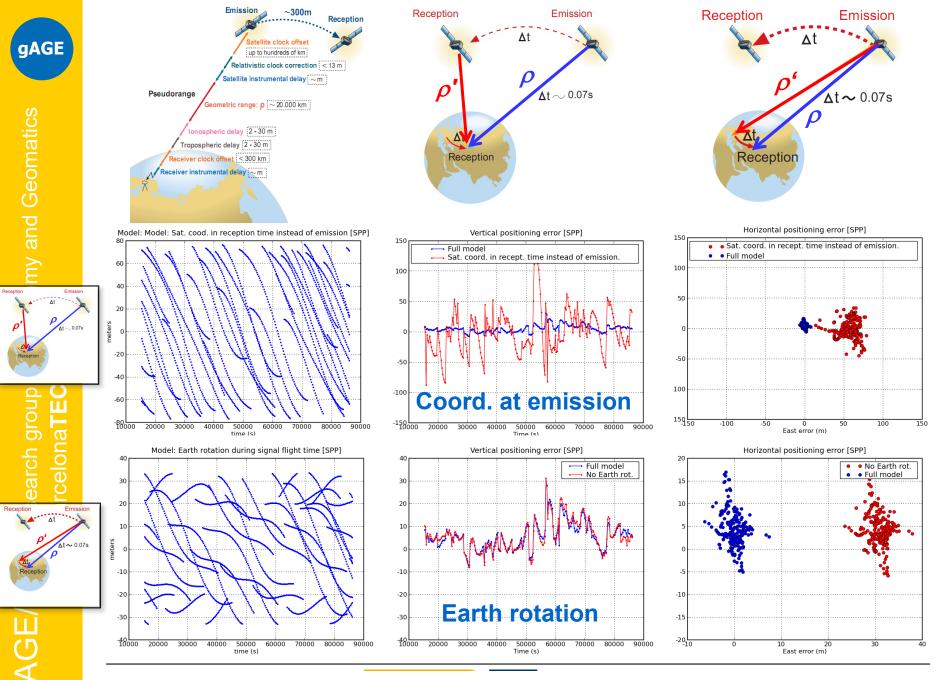
After this summary, we will focus on the additional modelling need for Precise Point Positioning.

Remember that the error component most difficult to model is the ionosphere. But, in the PPP technique the ionosphere error is removed (more than 99.9%) using dual-frequency measurements in the ionosphere-free combination (Lc,Pc). This combination also removes the Differential Code Bias (or TGD).

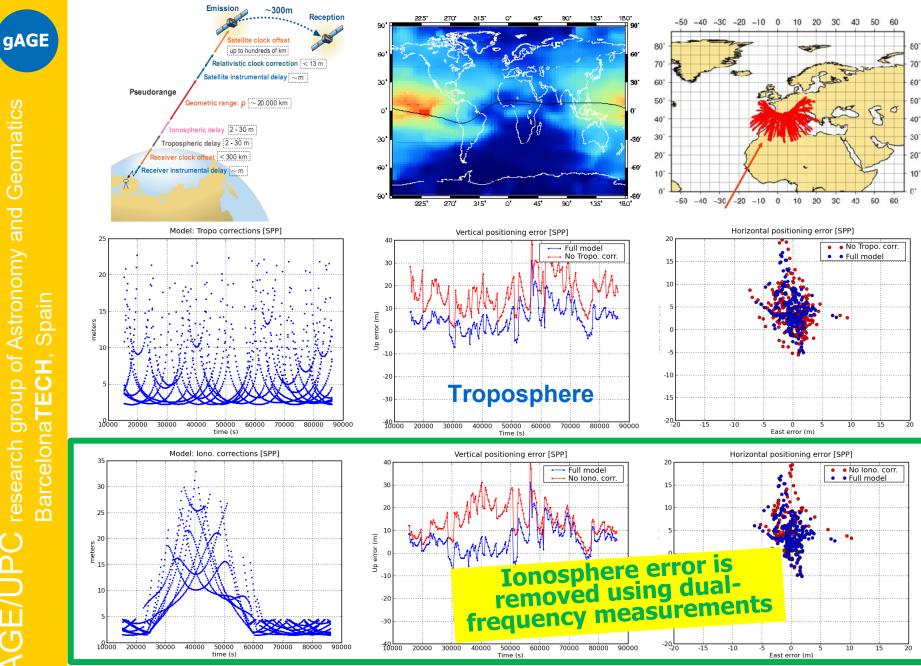


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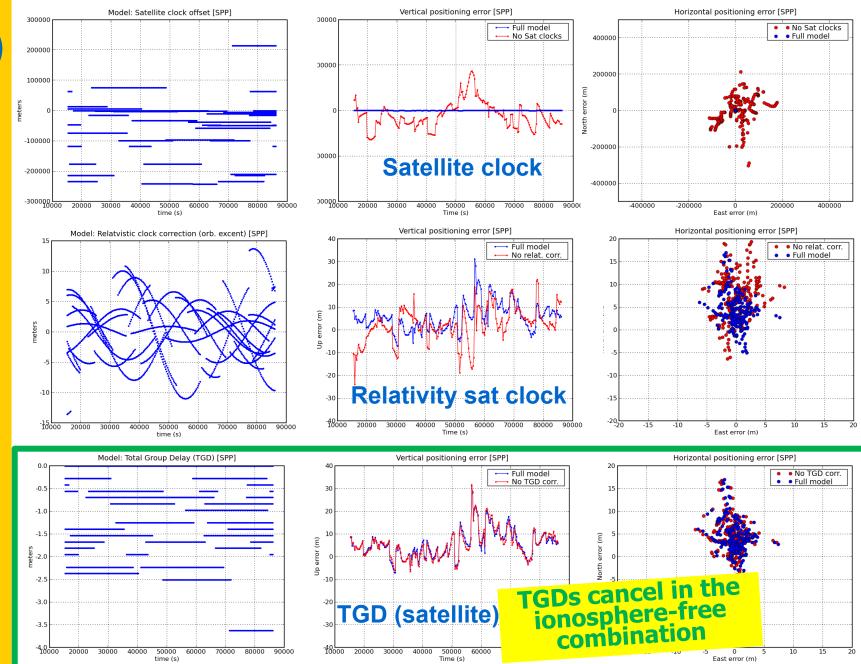
Satellite coordinates computation at signal emission time



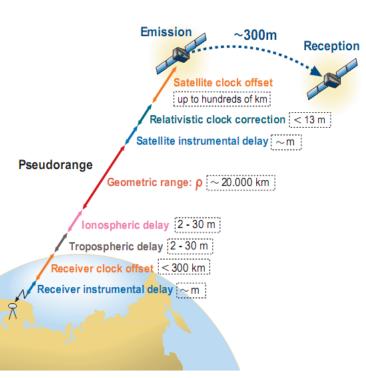
Signal propagation errors on the Atmosphere



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Satellite clocks and Total Group Delay (TGD)



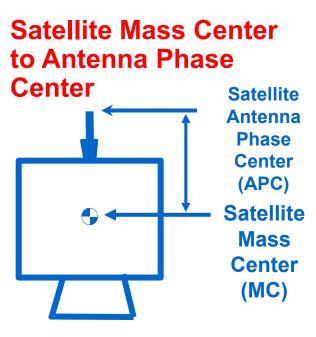
The PPP technique allows centimetrelevel of accuracy to be achieved for static positioning and decimetre level, or better, for kinematic navigation. This high accuracy requires an accurate **modelling "up to the centimetre level or better"**, where all previous model terms must be taken into account (except ionosphere and TGD [*]), **plus some additional terms given next:**

[*] Remember that in the PPP technique the ionosphere error is removed (more than 99.9%) using dual-frequency measurements in the ionospherefree combination (Lc,Pc). This combination also removes the Differential Code Bias (or TGD).



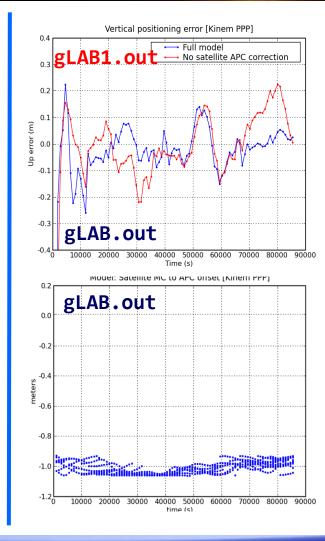
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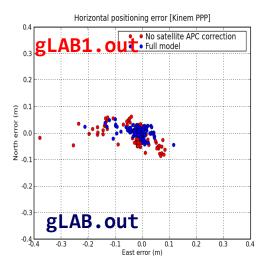
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Broadcast orbits are referred to the antenna phase center, but IGS precise orbits are referred to the satellite mass center.

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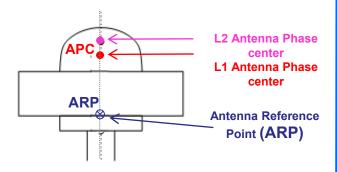
Satellite MC to APC:

The satellite MC to APC eccentricity vector depends on the satellite. The APC values used in the IGS orbits and clocks products are referred to the iono-free combination (LC, PC). They are given in the IGS ANTEX files (e.g., igs05.atx).



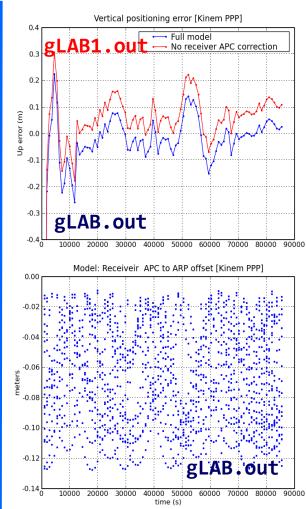


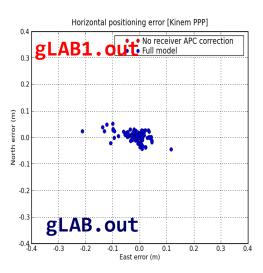
Receiver Antenna Phase center (APC)



GNSS measurements are referred to the APC. This is not necessarily the geometric center of the antenna, and it depends on the signal frequency and the incoming radio signal direction.

For geodetic positioning a reference tied to the antenna (ARP) or to monument is used





Receiver APC:

The antenna used for this experiment, has the APC position vertically shifted regarding ARP.

Thence, neglecting this correction, an error on the vertical component occurs, but not in the horizontal one.



Research group of Astronomy & Geomatics Technical University of Catalonia

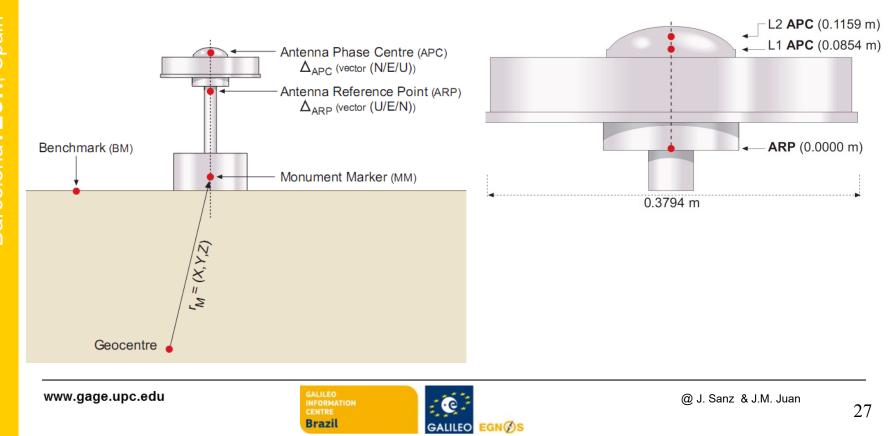


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Tutorial associated to the **GNSS Data Processing** book J. Sanz Subirana, J.M. Juan Zornoza, M. Hernández-Pajares

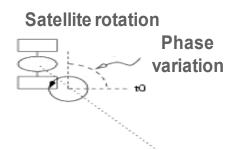
Antenna biases and orientation:

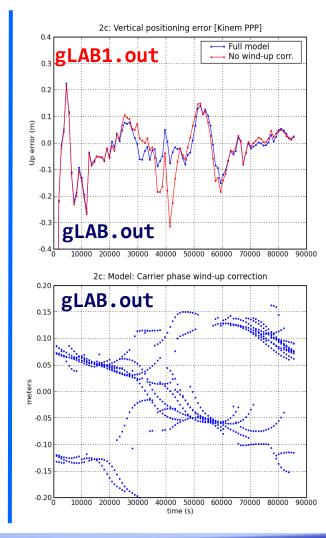
- The satellite and receiver **antenna phase centres (APCs)** can be found in the IGS ANTEX files, after GPS week 1400 (Nov. 2006)
- The **carrier phase wind-up** effect due to the satellite's motion must be taken into account.

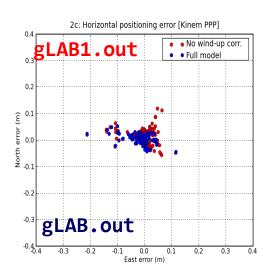


Wind-up affects only carrier phase. It is due to the electromagnetic nature of circularly polarized waves of GNSS signals.

As the satellite moves along its orbital path, it performs a rotation to keep its solar panels pointing to the Sun direction. This rotation causes a carrier variation, and thence, a range measurement variation.







Wind-Up

Wind-up changes smoothly along continuous carrier phase arcs.

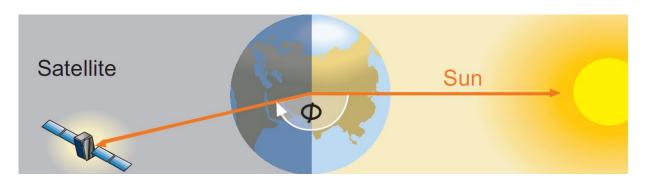
In the position domain, windup affects both vertical and horizontal components.





Tutorial associated to the **GNSS Data Processing** book J. Sanz Subirana, J.M. Juan Zornoza, M. Hernández-Pajares

Additional Modelling for PPP: Eclipse condition



High-accuracy GNSS positioning degrades during the GNSS satellites' eclipse seasons.

- Once the satellite goes into shadow, the radiation pressure vanishes. This effect introduces errors in the satellite dynamics due to the difficulty of properly modelling the solar radiation pressure.
- On the other hand, the satellite's solar sensors lose sight of the Sun and the attitude control (trying to keep the panels facing the Sun).

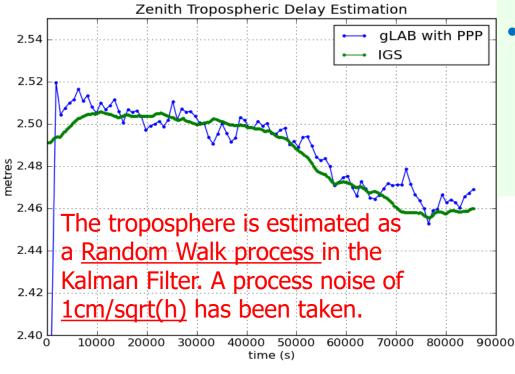
As a consequence, the orbit during shadow and eclipse periods may be considerably degraded and the removal of satellites under such conditions can improve the high-accuracy positioning results.



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Additional Modelling for PPP: Atmospheric Effects

- The ionospheric refraction and TGDs are removed using the ionosphere-free combination of code and carrier measurements (PC, LC).
- The tropospheric refraction can be modelled by Dry and Wet components (and different mappings are usually used for both components, e.g. mapping of Niell).



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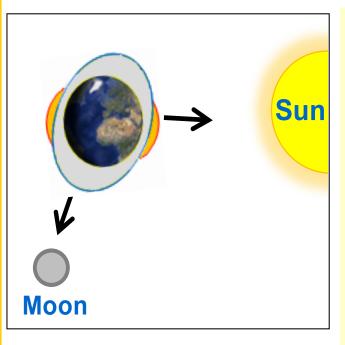
A residual tropospheric delay is estimated (as wet ZTD delay) in the Kalman filter, together with the coordinates, clock and carrier phase ambiguities.



Additional Modelling for PPP: Earth Deformation

Earth deformation effects:

- Solid tides must be modelled by equations
- Ocean loading and pole tides are second-order effects and can be neglected for PPP accuracies at the centimetre level

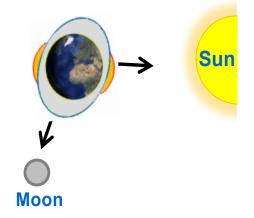


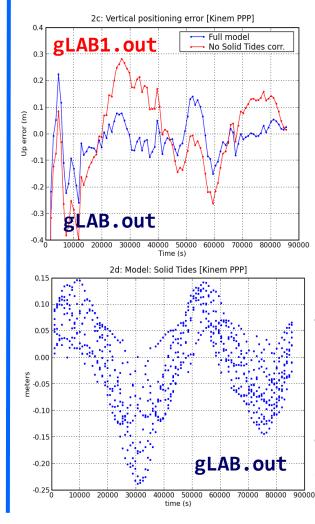
Solid Tides concern the movement of Earth's crust (and thus the variation in the receiver's location coordinates) due to gravitational attractive forces produced by external bodies, mainly the Sun and Moon. Solid tides produce vertical and horizontal displacements that can be expressed by the spherical harmonics expansion (m, n), characterised by the Love and Shida numbers h_{mn} and l_{mn} .

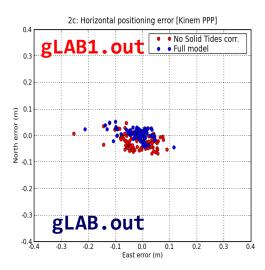


Solid Tides

It comprises the Earth's crust movement (and thence receiver coordinates variations) due to the gravitational attraction forces produced by external bodies, mainly the Sun and the Moon.







Solid Tides:

These effects do not affect the GNSS signals, but if they were not considered, the station coordinates would oscillate with relation to a mean value.

They produce vertical (mainly) and horizontal displacements.





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Linear observation model for PPP

It is based code and carrier measurements in the ionosphere-free combination (Pc, Lc), which are modelled as follows:



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$$P_{Crec}^{sat} = \rho_{rec}^{sat} + c \cdot (dt_{rec} - dt^{sat}) + Trop_{rec}^{sat} + \mathcal{M}_{Pc} + \varepsilon_{P_c}$$

 $L_{Crec}^{sat} = \rho_{rec}^{sat} + c \cdot (dt_{rec} - dt^{sat}) + Trop_{rec}^{sat} + \lambda_N \omega_{rec}^{sat} + B_{Crec}^{sat} + \mathcal{M}_{L_c} + \varepsilon_{L_c}$

where

$$P_{C} = \frac{f_{1}^{2}P_{1} - f_{2}^{2}P_{2}}{f_{1}^{2} - f_{2}^{2}}; \quad L_{C} = \frac{f_{1}^{2}L_{1} - f_{2}^{2}L_{2}}{f_{1}^{2} - f_{2}^{2}}$$

$$B_{C} = \lambda_{N} \left(B_{1} + \frac{\lambda_{W}}{\lambda_{2}} B_{W} \right)$$
$$B_{W} = B_{1} - B_{2}$$

Ionosphere is removed

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 $\lambda_N = 10.7 \text{ cm}, \lambda_W = 86.2 \text{ cm}$

Remark, ρ is referred to the Antenna Phase Centres (APC) of satellite and receiver antennas in the ionosphere free combination.

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Linear model: For each satellite in view

$$P_{C rec}^{sat} = \rho_{rec}^{sat} + c \cdot (dt_{rec} - dt^{sat}) + Trop + \varepsilon$$

Linearising ρ around an 'a priori' receiver position $(x_{rec,0}, y_{rec,0}, z_{rec,0})$

$$=\rho_{rec,o}^{sat} + \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}}\Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}}\Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}}\Delta z_{rec} + c\left(dt_{rec} - dt^{sat}\right) + Trop$$

where:

$$\Delta x_{rec} = x_{rec} - x_{rec,o}$$
; $\Delta y_{rec} = y_{rec} - y_{rec,o}$; $\Delta z_{rec} = z_{rec} - z_{rec,o}$

and taking: $Trop_{rec}^{sat} = Trop_{0 rec}^{sat} + M_{wet, rec}^{sat} \Delta Tr_{Z, wet}$

 $+ c dt_{rec}$

 $+ M_{wet}^{sat} \Delta Tr_{Z,wet}$

Prefit-residuals (Prefit) $P_{C rec}^{sat} - \rho_{rec,o}^{sat} + c dt^{sat} - Trop_{0rec}^{sat} = \frac{x_{rec,o} - x^{sat}}{c^{sat}}$ $Z_{rec,o} - Z^{sa}$ $y_{rec,o} - y^{st}$ $-\Delta x_{rec}$ $(\Delta y_{rec}) +$ ΔZ_{rec} $\rho_{rec.o}^{sat}$ $\rho_{rec.o}^{sat}$ $ho^{\scriptscriptstyle sat}_{\scriptscriptstyle rec,o}$ knówn IIN computed measurement The same for carrier, but adding the ambiguity as an unknown

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Remark $P_{C rec}^{sat} = \rho_{rec}^{sat} + c \cdot (dt_{rec} - dt^{sat}) + Trop + \varepsilon$

Linearising ρ around an 'a priori' receiver position $(x_{rec,0}, y_{rec,0}, z_{rec,0})$

$$=\rho_{rec,o}^{sat} + \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}} \Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}} \Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}} \Delta z_{rec} + c\left(dt_{rec} - dt^{sat}\right) + Trop$$

Of course, receiver coordinates $(x_{rec}, y_{rec}, z_{rec})$ are not known (they are the target of this problem). But, we can always assume that an "approximate position $(x_{0,rec}, y_{0,rec}, z_{0,rec})$ is known".

Thence, the navigation problem will consist on:

1.- To start from an approximate value for receiver position

 $(x_{0,rec}, y_{0,rec}, z_{0,rec})$ e.g. the Earth's centre) to linearise the equations 2.- With the pseudorange measurements and the ravigation equations, compute the correction $(\Delta x_{rec}, \Delta y_{rec}, \Delta z_{rec})$ to have improved estimates: $(x_{rec}, y_{rec}, z_{rec}) = (x_{0,rec}, y_{0,rec}, z_{0,rec}) + (\Delta x_{rec}, \Delta y_{rec}, \Delta z_{rec})$

3.- Linearise the equations again, about the new improved estimates, and iterate until the change in the solution estimates is small enough.

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Linear model: For each satellite in view

$$P_{C rec}^{sat} = \rho_{rec}^{sat} + c \cdot (dt_{rec} - dt^{sat}) + Trop + \varepsilon$$

Linearising ρ around an 'a priori' receiver position $(x_{rec,0}, y_{rec,0}, z_{rec,0})$

$$=\rho_{rec,o}^{sat} + \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}}\Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}}\Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}}\Delta z_{rec} + c\left(dt_{rec} - dt^{sat}\right) + Trop$$

where:

$$\Delta x_{rec} = x_{rec} - x_{rec,o} \quad ; \quad \Delta y_{rec} = y_{rec} - y_{rec,o} \quad ; \quad \Delta z_{rec} = z_{rec} - z_{rec,o}$$

and taking: $Trop_{rec}^{sat} = Trop_{0 rec}^{sat} + M_{wet, rec}^{sat} \Delta Tr_{Z, wet}$

 $+ c dt_{rec}$

 $+ M_{wet}^{sat} \Delta Tr_{z,wet}$

Prefit-residuals (Prefit) $P_{C rec}^{sat} - \rho_{rec,o}^{sat} + c dt^{sat} - Trop_{0rec}^{sat} = \frac{x_{rec,o} - x^{sat}}{c^{sat}}$ $Z_{rec,o} - Z^{sa}$ $y_{rec,o} - y^{st}$ $-\Delta x_{rec}$ $(\Delta y_{rec})^{+}$ ΔZ_{rec} $\rho_{rec.o}^{sat}$ $\rho_{rec.o}^{sat}$ $ho^{\scriptscriptstyle sat}_{\scriptscriptstyle rec,o}$ knówn IIN computed measurement The same for carrier, but adding the ambiguity as an unknown

Linear model: For each satellite in view

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Linearising ρ around an 'a priori' receiver position $(x_{rec,0}, y_{rec,0}, z_{rec,0})$

$$=\rho_{rec,o}^{sat} + \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}} \Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}} \Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}} \Delta z_{rec} + c\left(dt_{rec} - dt^{sat}\right) + Trop$$

where:

Prefit-residuals (Prefit)

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$$\Delta x_{rec} = x_{rec} - x_{rec,o} \quad ; \quad \Delta y_{rec} = y_{rec} - y_{rec,o} \quad ; \quad \Delta z_{rec} = z_{rec} - z_{rec,o}$$

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and taking: $Trop_{rec}^{sat} = Trop_{0 rec}^{sat} + M_{wet, rec}^{sat} \Delta Tr_{Z, wet}$

$$P_{C \ rec}^{sat} - \rho_{rec,o}^{sat} + c \ dt^{sat} - Trop_{0rec}^{sat} = \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}} \Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}} \Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}} \Delta z_{rec} + C \ dt_{rec} + M_{wet}^{sat} \Delta Tr_{z,wet}$$

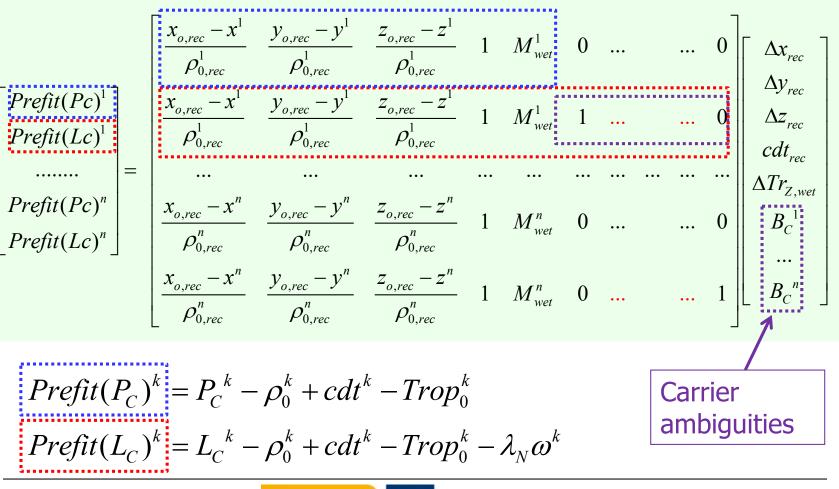
$$L_{C \ rec}^{sat} - \rho_{rec,o}^{sat} + c \ dt^{sat} - Trop_{0rec}^{sat} - \lambda_{N} \omega^{sat} = \frac{x_{rec,o} - x^{sat}}{\rho_{rec,o}^{sat}} \Delta x_{rec} + \frac{y_{rec,o} - y^{sat}}{\rho_{rec,o}^{sat}} \Delta y_{rec} + \frac{z_{rec,o} - z^{sat}}{\rho_{rec,o}^{sat}} \Delta z_{rec} + C \ dt_{rec} + M_{wet}^{sat} \Delta Tr_{z,wet} + B_{c}^{sat}$$

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Following the same procedure as with the code based positioning (SPP), the linear observation model y = G xfor the code and carrier measurements can be written as follows: y = G x



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@ J. Sanz & J.M. Juan

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Parameter estimation PPP: Floating Ambiguities

The linear observation model y = G x can be solved using the Kalman filter. The next stochastic model can be used

- Carrier phase ambiguities (B_C) are taken as 'constant' along continuous phase arcs, and as `white noise' when a cycle slip happens (σ= 10⁴ m can be taken, for instance) → FLOATED AMB.
- Wet tropospheric delay $(Tr_{z;wet})$ is taken as a random walk process (with $d\sigma^2/dt = 1 \ cm^2/h$, for instance).
- **Receiver clock** (*cdt*) is taken as a white-noise process

(with $\sigma = 3.10^5 m$, i.e. 1 ms for instance).

- Receiver coordinates ($\Delta x, \Delta y, \Delta z$)
 - For static positioning the coordinates are taken as constants.
 - For kinematic positioning the coordinates are taken as white noise or a random walk process.

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Comment: Floating Ambiguities

This solution procedure is called **floating ambiguities**. 'Floating' in the sense that the ambiguities are estimated by the filter 'as real numbers'.

The bias estimations \hat{B}_{C} will converge to a solution after a transition time that depends on the observation geometry, model quality and data noise.

In general, one must expect errors at the decimetre level, or better, in pure kinematic positioning (after the best part of one hour) and at the centimetre level in static PPP over 24h data.

See exercises in the laboratory session (Tutorial 1).

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Carrier Ambiguity Fixing concept

In the previous formulation, the ambiguities have been estimated as real numbers in the Kalman filter, without exploiting its integer nature.

That is, the ambiguities in L_1 , L_2 or L_W signals are an integer number (*N*) of its associated wavelength (λ) plus a fractional part associated to the satellite and to the receiver.

$$B_{1,rec}^{sat} = \lambda_1 N_{1,rec}^{sat} + b_{1,rec} + b_1^{sat}$$
$$B_{2,rec}^{sat} = \lambda_2 N_{2,rec}^{sat} + b_{2,rec} + b_2^{sat}$$
$$N_W = N_I - N_2$$

$$B_{C} = \lambda_{N} \left(N_{1} + \frac{\lambda_{w}}{\lambda_{2}} N_{W} \right) + b_{C,rec} + b_{C}^{sat}$$

Bc is not an integer number of λ_N but can be related with the integers N_I , N_W

The Ambiguity Fixing techniques take benefit of this INTEGER NATURE of N_1 , N_2 ambiguities to properly fix them, reducing convergence time, and thence, achieving high accuracy quickly.

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Carrier Ambiguity Fixing concept

Two different approaches can be considered:

• Double differenced Ambiguity Fixing (e.g. RTK):

This is the classical approach which relies in the fact that the fractional part of carrier ambiguities cancels when forming the double differences between receivers and satellites:

That is, given:
$$B_{rec}^{sat} = \lambda N_{rec}^{sat} + b_{rec} + b^{sat}$$

The double differences, regarding a reference receiver and satellite, yield: $\Delta \nabla B_{rec}^{sat} = B_{rec}^{sat} - B_{rec,R}^{sat} - \left(B_{rec}^{sat,R} - B_{rec,R}^{sat,R}\right) = \lambda \Delta \nabla N_{rec}^{sat}$

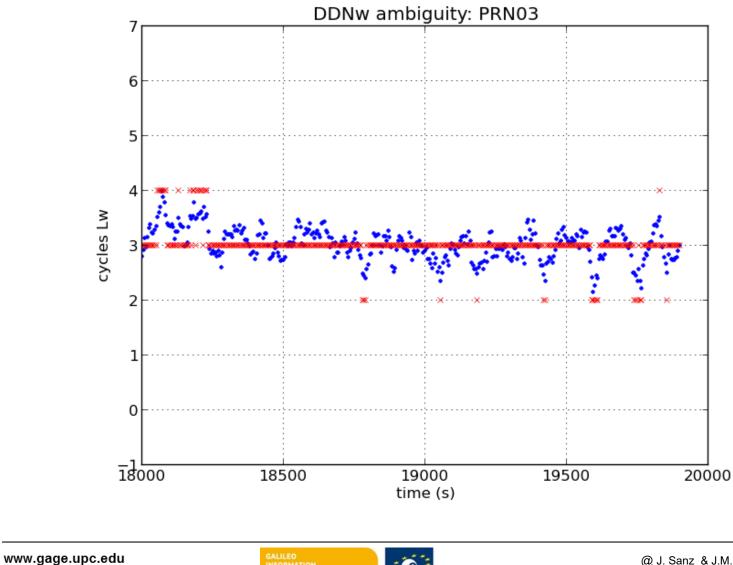
where the satellite and receiver ambiguity terms (b_{rec} , b^{sat}) cancel out.

• Absolute (or undifferenced) ambiguity fixing (e.g. PPP AR):





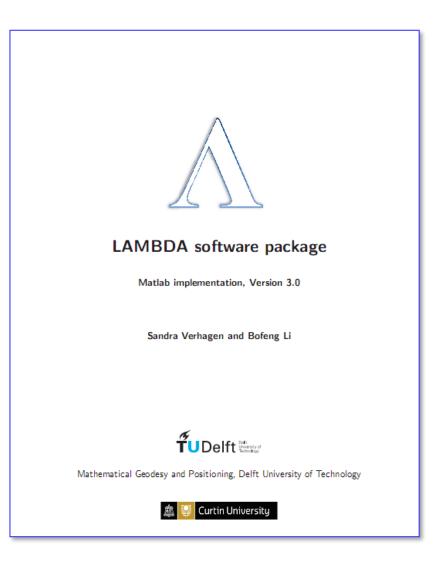
Example of Ambiguity Fixing by rounding



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The LAMBDA METHOD



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Carrier Ambiguity Fixing concept

Two different approaches can be considered:

• Double differenced Ambiguity Fixing (e.g. RTK):

This is the classical approach which relies in the fact that the fractional part of carrier ambiguities cancels when forming the double differences between receivers and satellites:

→ That is, given: $B_{rec}^{sat} = \lambda N_{rec}^{sat} + b_{rec} + b^{sat}$ The double differences, regarding a reference receiver and satellite, yield: $\Delta \nabla B_{rec}^{sat} = B_{rec}^{sat} - B_{rec,R}^{sat} - (B_{rec}^{sat,R} - B_{rec,R}^{sat,R}) = \lambda \Delta \nabla N_{rec}^{sat}$

Absolute (or undifferenced) ambiguity fixing (e.g. PPP AR):

This is a new approach, where the fractional part of the ambiguities are estimated from a global network of permanent stations and provided to the users. Thus, the user can remove this fractional part and fix the remaining ambiguity as an integer number.

$$B_{rec}^{sat} = \lambda N_{rec}^{sat} + b_{rec} + b^{sat}$$

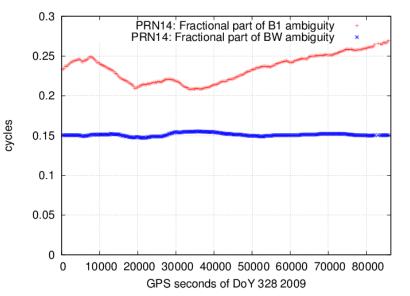
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Absolute (or undifferenced) ambiguity fixing

Nevertheless, these carrier hardware biases (or fractional part of carrier ambiguities) can be estimated together with the orbits, clocks, ionosphere and DCBs from measurements of a worldwide reference stations network.



These carrier hardware biases are slow varying parameters and can be broadcast to the user, together with the other differential corrections (orbits, clocks, ionosphere...) from a reference station network.

Then, the user can remove them and estimate the remaining ambiguities as integer numbers.

This can allow world-wide PPP users to perform ambiguity fixing, without baseline length limitation, improving accuracy and reducing convergence time.

Note: These carrier hardware biases are canceled in RTK when forming Double-Differences of measurements between pairs of satellites and receivers.

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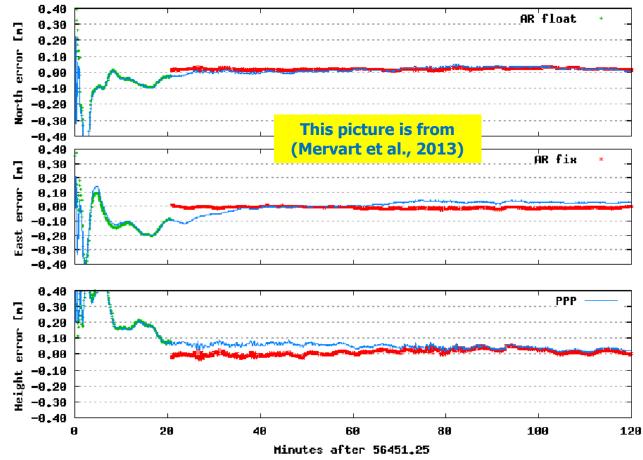


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June 2013



The main weakness of PPP is the large convergence time, which depend on satellites geometry, quality of data (code noise, cycle-slips...). There is a sudden improvement when fixing carrier ambiguities, but still several tens of minutes are needed to achieve centimeter level of accuracy.

L. Mervart, C. Rocken, T. Iwabuchi, Z. Lukes and M. Kanzaki (2013). Precise Point Positioning with Fast Ambiguity Resolution – Prerequisites, Algorithms and Performance. *Proceedings of the 27th International Technical Meeting of The Satellite Division of the Institute of Navigation (ION GNSS+ 2013), Nashville, Tennessee, September 16-20, 2013.*

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Precise Point Positioning (PPP)

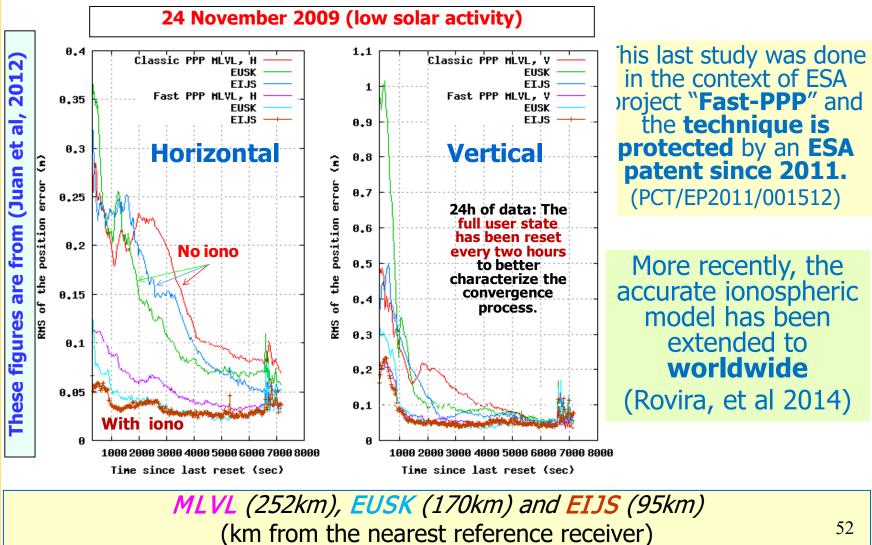
- 1. Introduction
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Fast-PPP: Accelerating convergence with IONO

• During the early 2000s gAGE/UPC developed a two layers grid model, and afterwards assessed its suitability to help the PPP convergence.

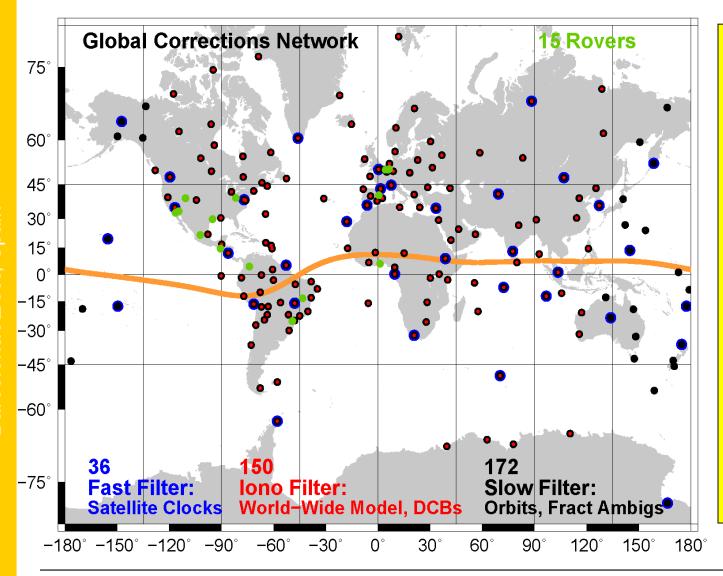


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Actual GNSS Data the entire Year 2014

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World wide Iono. model

Rovers are located at distances are orders of magnitude greater than RTK baselines

Close to maximum Solar Cycle conditions

Moderate Geomagnetic Dst Values

- How the ionosphere helps the filter convergence in Fast-PPP?
 - →In the classical PPP, the navigation filter convergence is driven by the convergence of the floated iono-free ambiguity (B_C), which, at the beginning, depends on the code noise.
 - 1) There is a constraint between the <u>wide-lane</u> ambiguity (B_{W}), the <u>iono-free</u> ambiguity (B_{C}) and the <u>ionospheric refraction</u> (*STEC*) and *DCB*.

 $B_C = B_W - 1.98 (L_1 - L_2 - STEC - DCB)$

- 2) The <u>wide-lane</u> ambiguity ($B_{\nu\nu}$) is estimated/fixed quickly (~<u>5 minutes</u> with 2-freq and in <u>single epoch</u> with 3-freq. signals).
- 3) The <u>ionosphere</u> (*STEC*) is the bridge (through the mentioned constraint) to transfer the quick accuracy achieved in the <u>wide-lane ambiguity</u> ($B_{\nu\nu}$) computed value to the <u>iono-free ambiguity</u> (B_{c}) estimation, accelerating in this way the filter convergence.
- →Thence, in Fast-PPP the convergence time is strongly reduced thanks to the quick wide-lane ambiguity fixing and the accurate ionospheric corrections. It allows to achieve High Accuracy quickly (~5 minutes with 2-freq & single epoch with 3-freq).

The ionosphere will help provided that its quality (noise/error) is better than the code

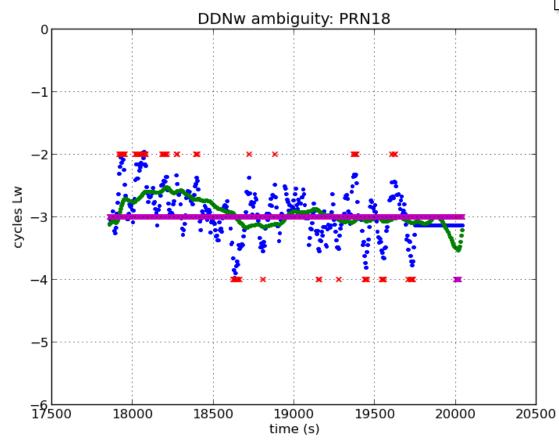
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300 seconds smoothing



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Thank you

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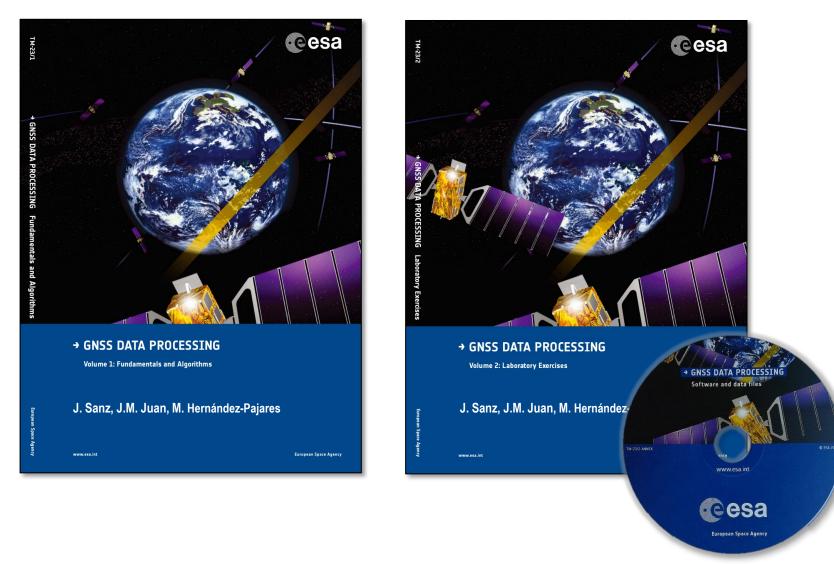


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GNSS Data Processing, Vol. 1: Fundamentals and Algorithms. GNSS Data Processing, Vol. 2: Laboratory exercises.

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Fast-PPP Ionospheric Model

1.- Derived from the geometry-free combination of **carrier-phases**:

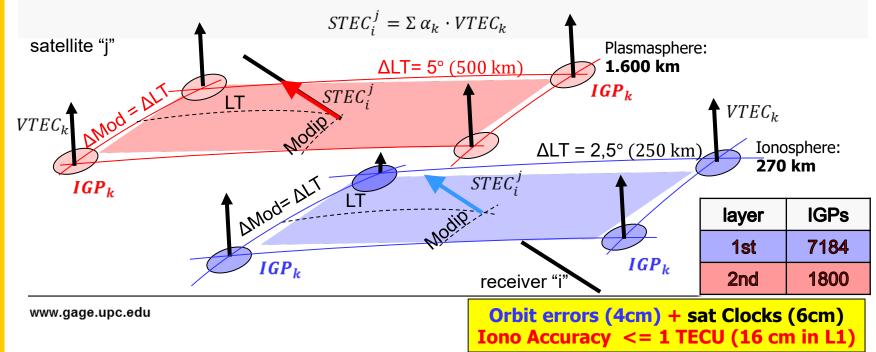
$$LI = L1 - L2$$

2.- Ambiguities are fixed (thanks to the CPF accurate geodetic modelling):

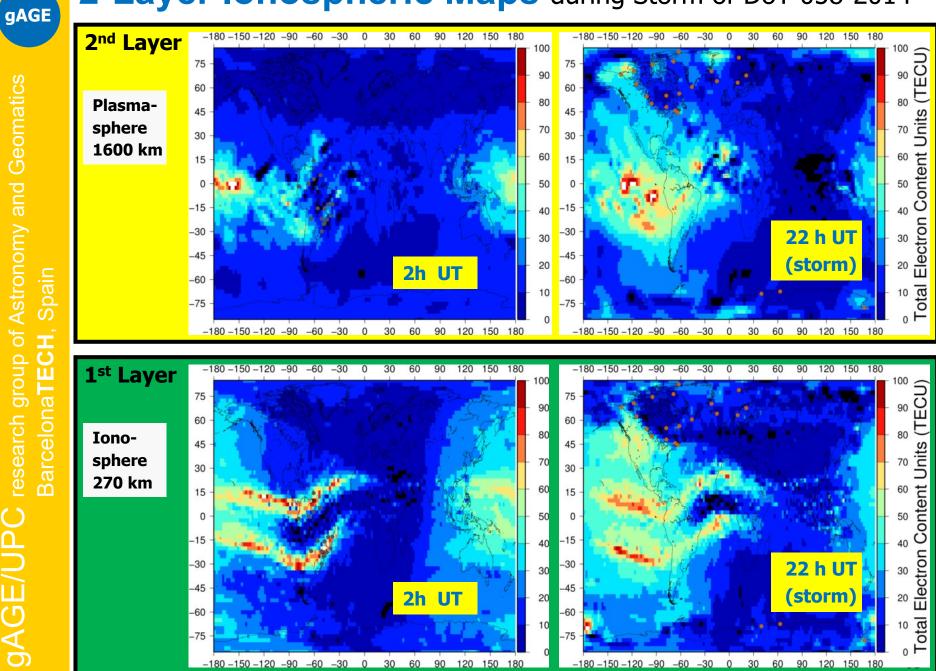
Unambiguous
$$LI_i^j - BI_i^j = STEC_i^j + DCB_i - DCB^j$$

Carrier phase noise (mm)

3.- The Slant Total Electron Content (STEC) is estimated with Vertical STEC (VTEC) on each "k" Ionospheric Grid Point (IGP) at the **two-layers**:

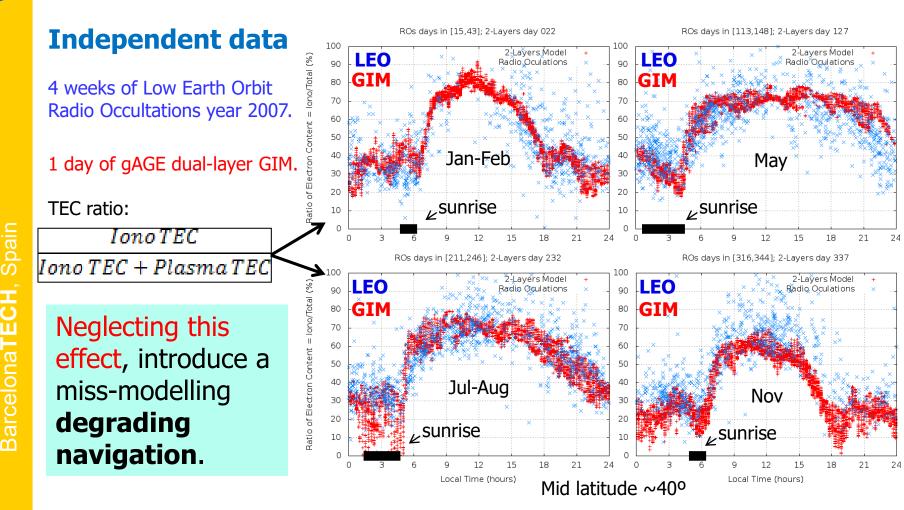


2-Layer lonospheric Maps during Storm of DoY 058-2014



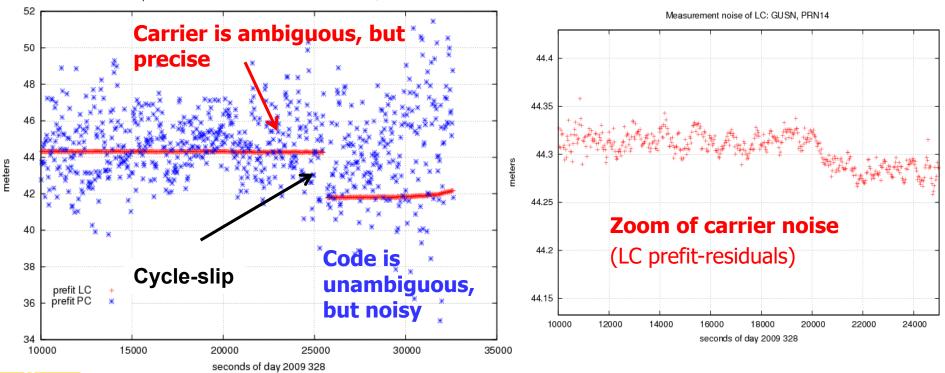
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Agreement Electron Contents of dual-layers between GIM derived from "earth" data and "space-borne" data



G. González-Casado, J. M. Juan, J. Sanz, A. Rovira-Garcia, and A. Aragon-Angel. "Determination of the Ionospheric and Plasmaspheric contributions to the Total Electron Content using Radio Occultations and Global Ionospheric Maps" Journal of Geophysical Research, 101002/2014JA020807.

Comparison of measurement noise of LC and PC: GUSN, PRN14



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- Code measurements are unambiguous but noisy (meter level noise).
- **Carrier** measurements are precise (few millimetres of noise) but ambiguous (the unknown ambiguities can reach thousands of km).
- Carrier phase ambiguities are estimated in the navigation filter along with the other parameters (coordinates, clock offsets, etc.). If these ambiguities were fixed, measurements accurate to the level of few millimetres would be available for positioning. However, some time is needed to decorrelate such ambiguities from the other parameters in the filter, and the estimated values are not fully unbiased.

